

# Lynx X-ray Grating Spectrometer

Ralf Heilmann<sup>1</sup> & Randy McEntaffer<sup>2</sup>

IWG Co-chairs and Grating Leads, on behalf of the IWG Grating Team

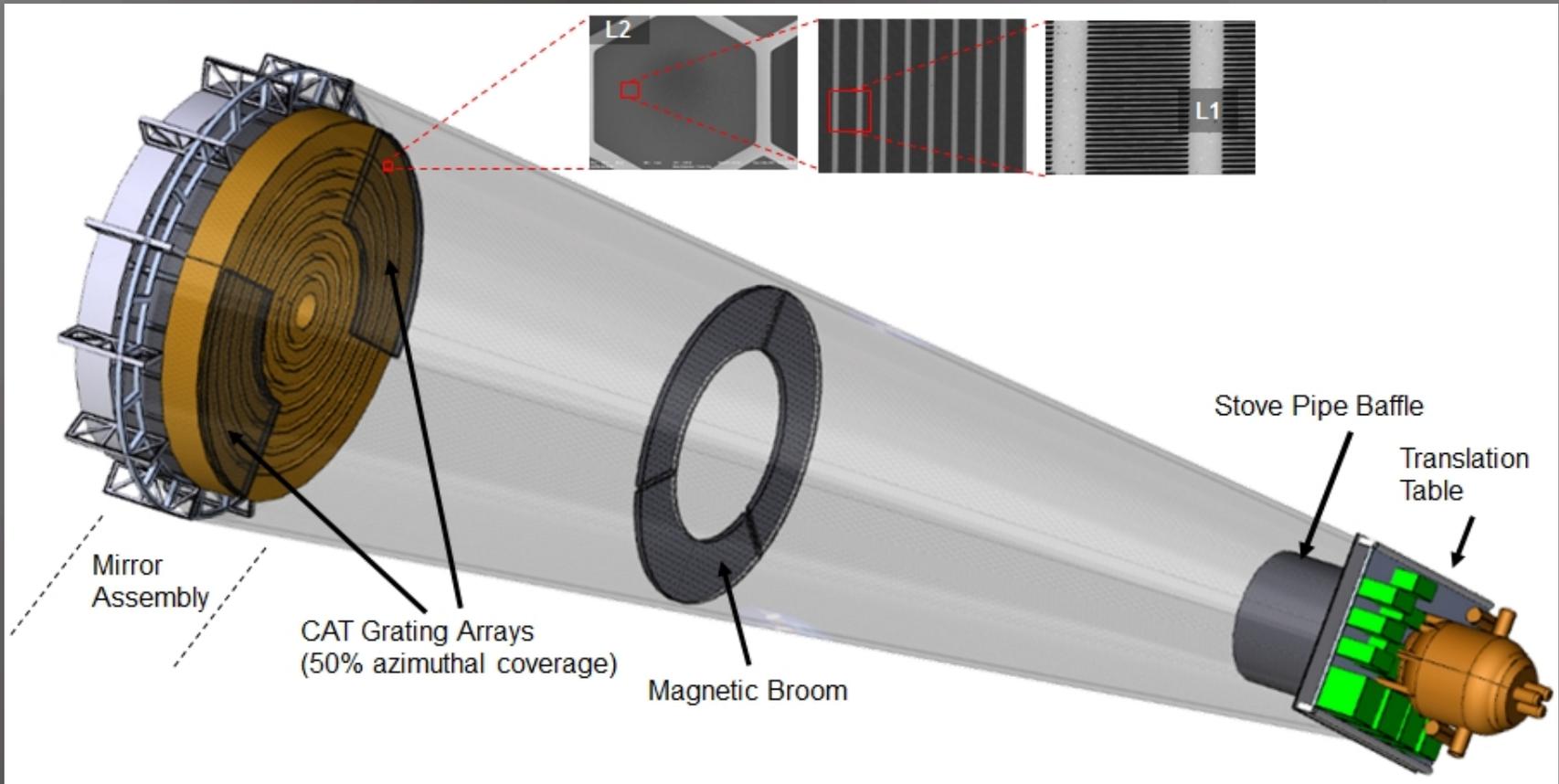
<sup>1</sup>MIT Kavli Institute for Astrophysics and Space Research

<sup>2</sup>Penn State University

# XGS Science topics/requirements

- Diffuse baryons
  - Census, mapping, metallicity in cosmic web
  - Content in galactic halos
  - Milky Way - rotational and turbulent velocity of hot halo gas
- Black holes
  - Kinematics and physical characteristics of warm absorbers near SMBHs
  - XRB and ULX spectroscopy, with some time resolution
- Stellar atmospheres
  - Photosphere absorption of neutron stars in GCs and SNR
  - Coronae and flares
  - Young star accretion
  - Winds around BHs (XRBs & ULXs)
- *Require  $R > 5000$ , effective area  $\sim 4000 \text{ cm}^2$*   
*soft X-rays: 0.2-2.0 keV*
- *These require further guidance from STDT*
- Can be addressed by Off-Plane Grating (OPG) and Critical Angle Transmission (CAT) grating technologies

# Grating Spectrometer Overview



- Removable grating arrays aft of mirrors
- Blazed gratings; only orders on one side are utilized (smaller readout).
- Fixed readout array in focal plane
- No low energy high-resolution spectroscopy on Athena

# CAT and OPG Spectrometers: Commonalities

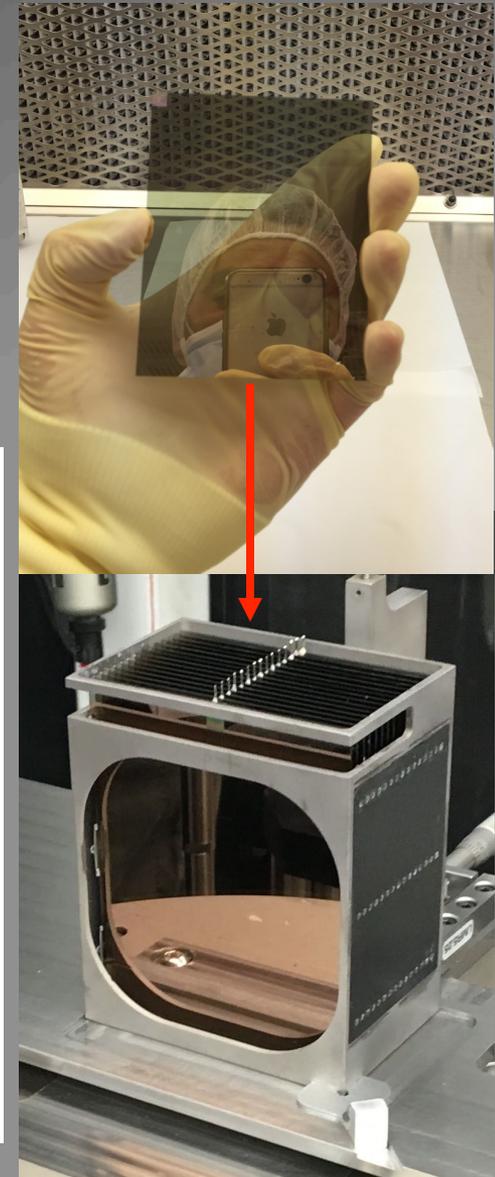
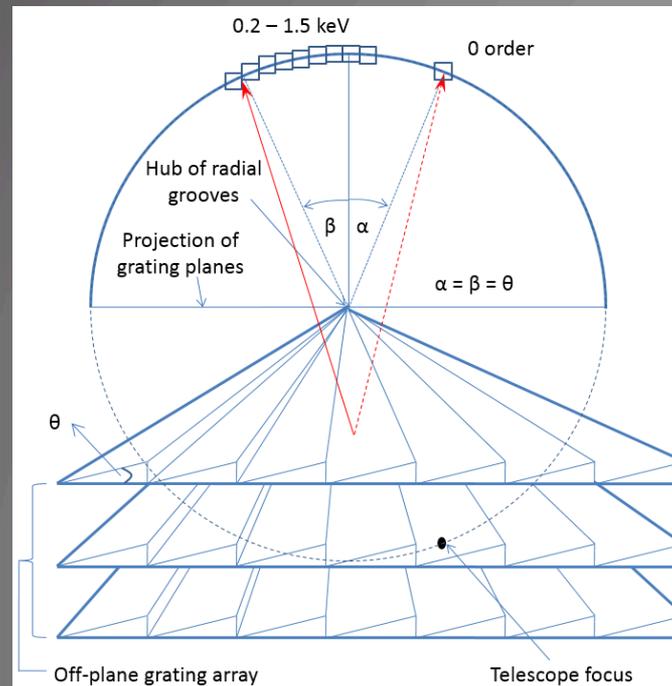
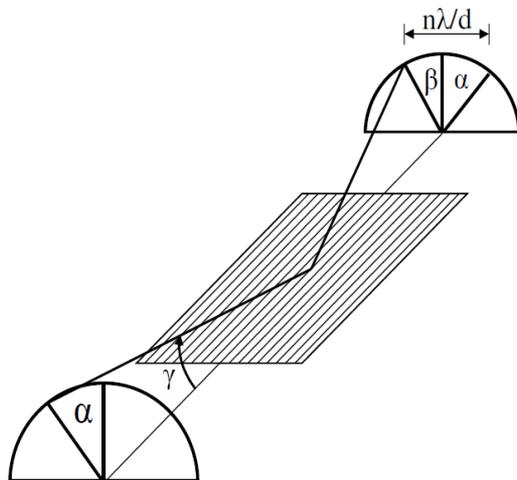
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- Blazing into higher orders/larger angles: Increased resolving power.
- Maximum resolving power: (Dispersion distance or “throw”)/(PSF plate scale projected onto dispersion axis).
- Sub-aperturing boosts resolving power.
- Aberrations reduce resolving power.
- High diffraction efficiency over broad band due to angles of grazing incidence onto grating surfaces being below the critical angle.
- Band limited on short wavelength side by critical angle.
- Different orders overlap spatially: detectors sort orders.
- Detector pixels oversample PSF.
- Tradeoff between short wavelength cutoff and resolving power.

# Off-Plane Gratings (OPGs)

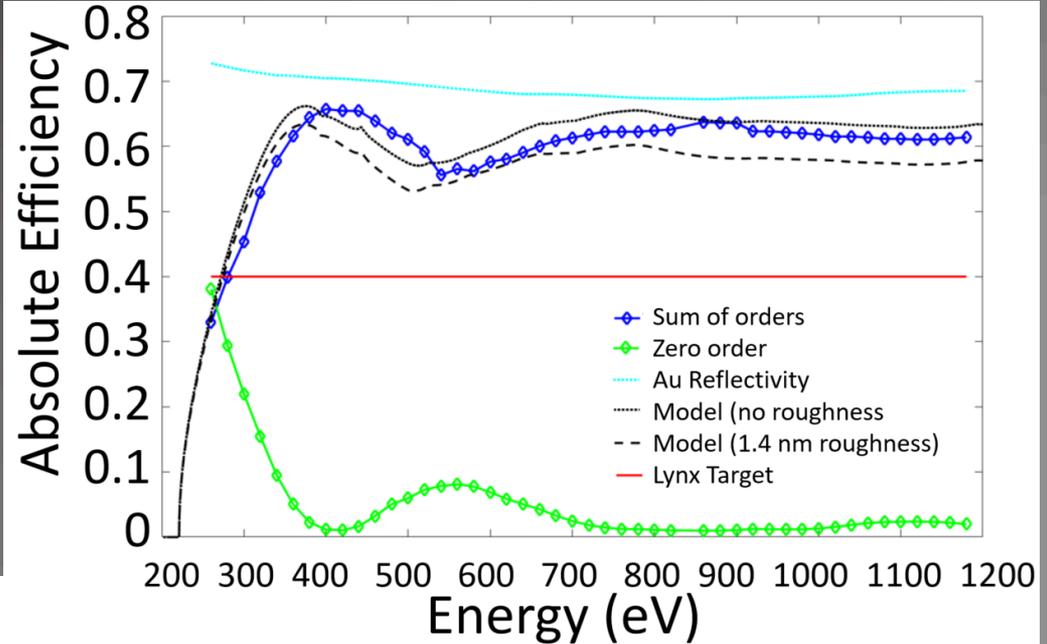
- Offer very high diffraction efficiency and high spectral resolving power
- Individual grating elements aligned into a grating module then integrated into a grating array behind the optics
- Require dedicated detector

$$\sin(\alpha) + \sin(\beta) = \frac{n\lambda}{d \sin(\gamma)}$$

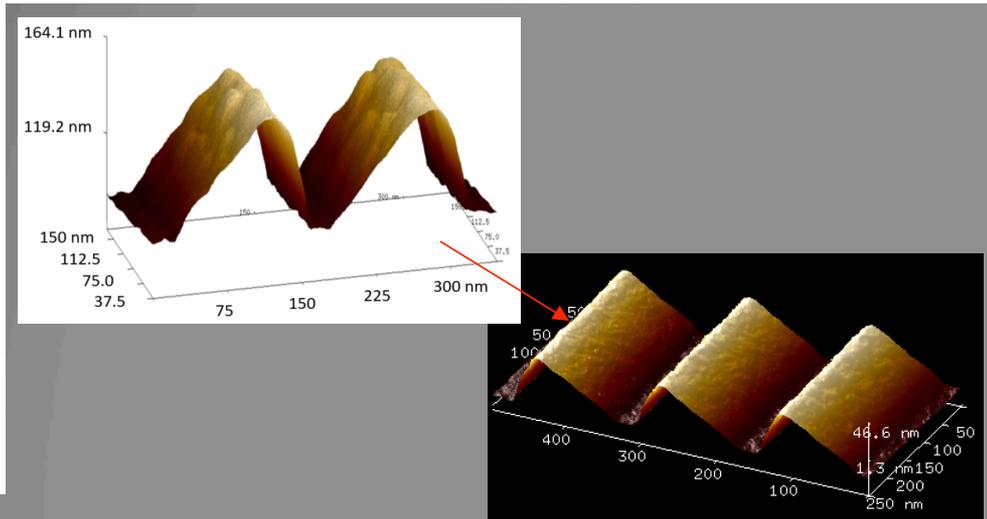
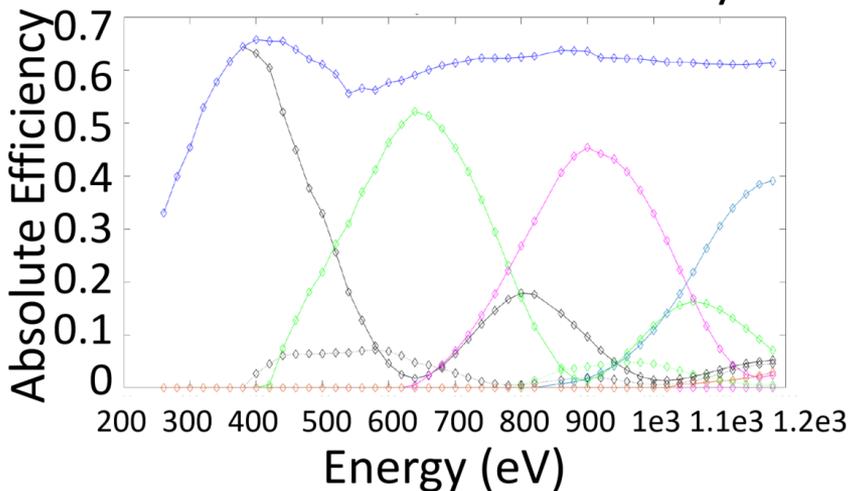


# OPG Diffraction Efficiency

- ~60% absolute diffraction efficiency over wide band
- High efficiency per order
- Low surface roughness
- Measure smoother facets over larger areas to approach 100% groove efficiency

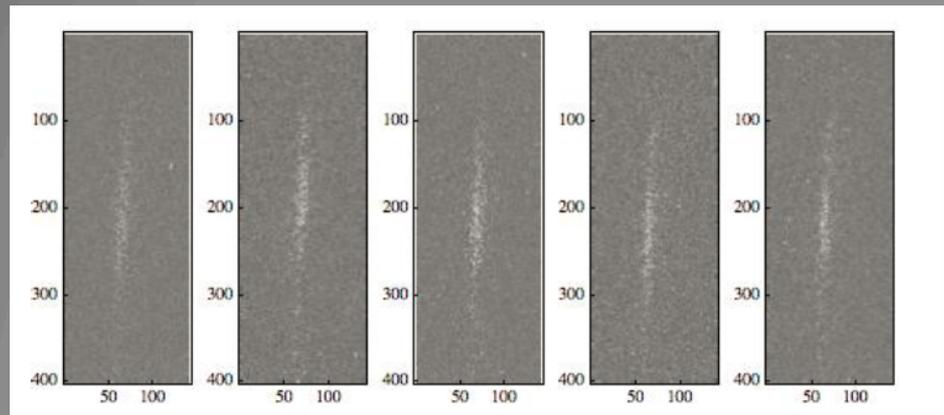
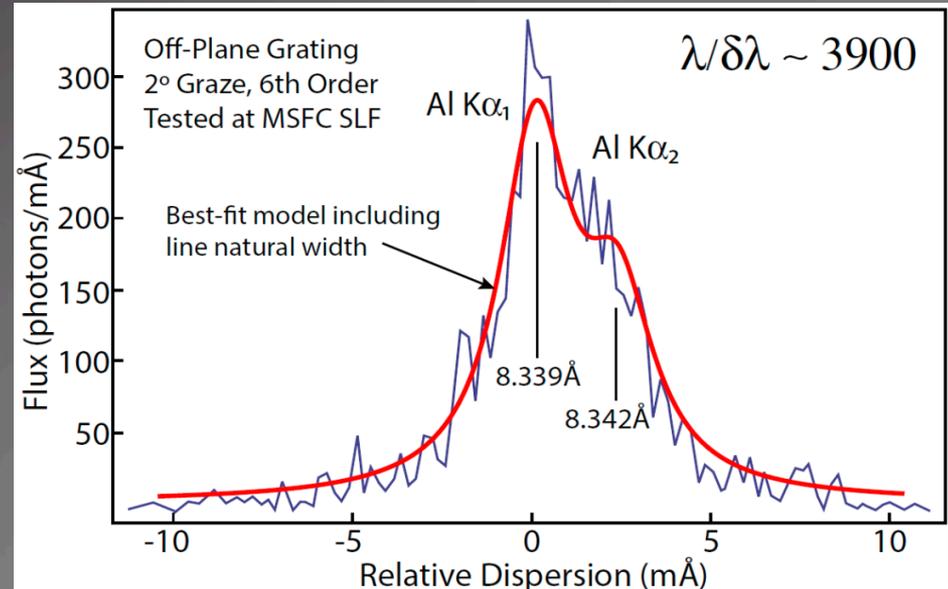


### Individual Order Efficiency



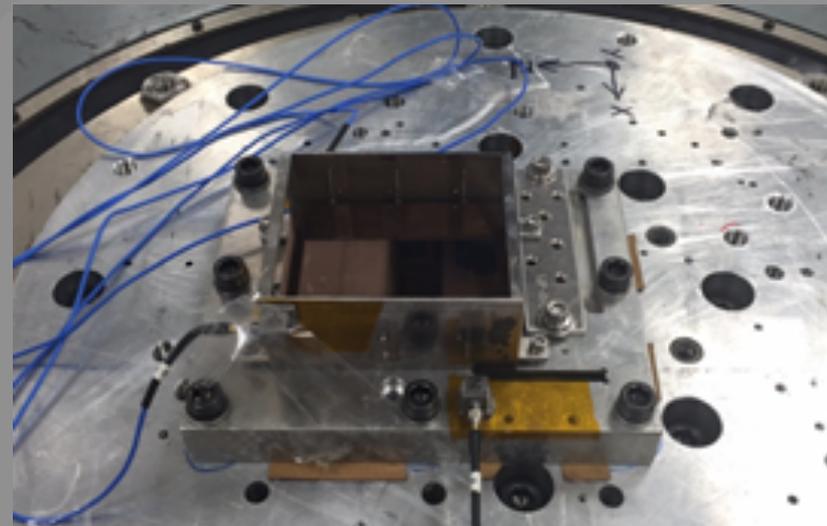
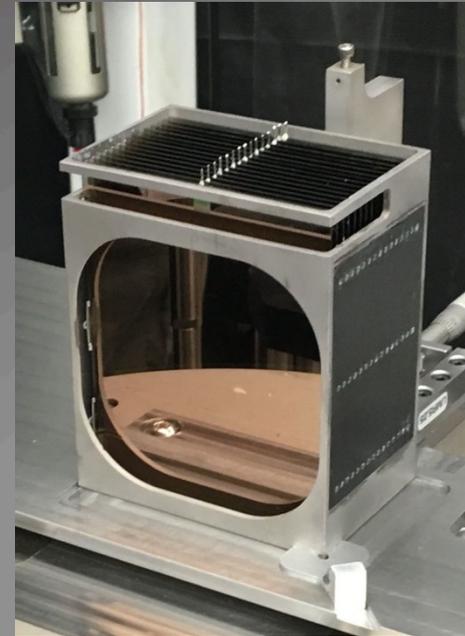
# OPG Spectral Resolving Power

- MSFC Stray Light Facility (SLF)
  - 6<sup>th</sup> order Al  $K\alpha_1$  and Al  $K\alpha_2$
  - Resolving power  $\sim 3900$  ( $\lambda/\delta\lambda$ )
    - After removing contributions from source size and natural line widths
  - Small format grating, 25 x 32 mm
  - Lamellar groove profile (no blaze)
  - Partial illumination
  
- Recent SLF test on large format grating (75 x 96 mm)
- Resolution limited to  $\sim 900$
- Fabrication errors need to be addressed



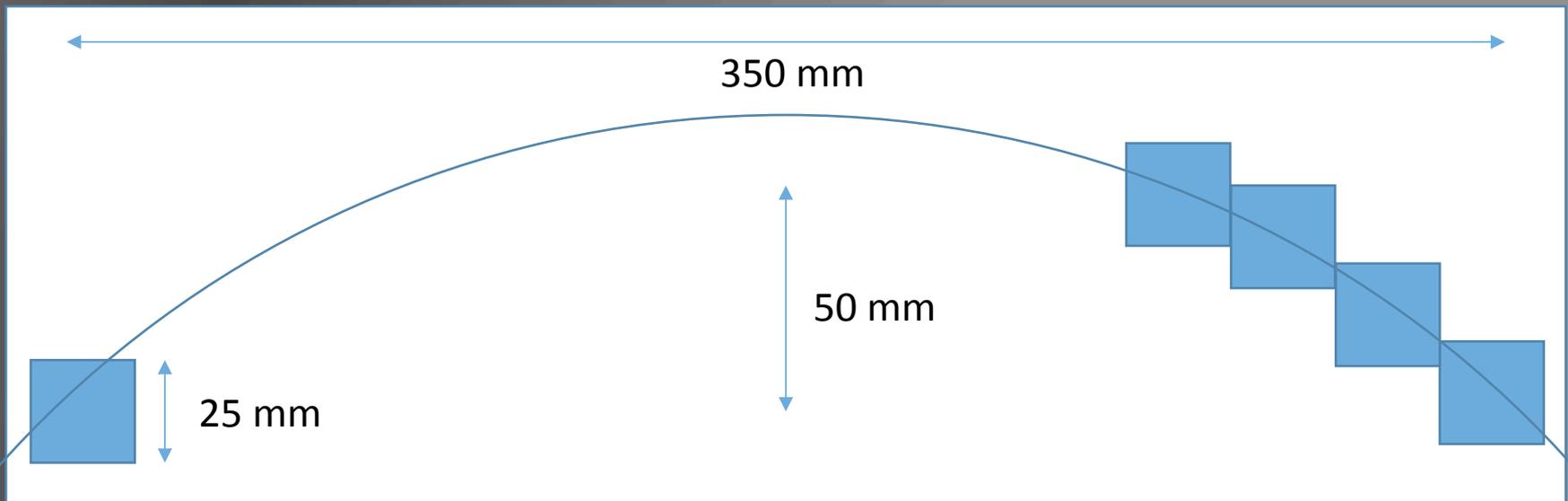
# OPG Alignment

- Optical alignment methods have been developed at PSU and SAO
- Modules have been aligned, performance tested and environmentally tested at full NASA GEVS levels, e.g.
  - Vibe Qualification
    - $\frac{1}{4}$  G sine sweep
    - 14.1 G RMS: Steps = [3, 5, 7.1, 10, 14.1] – 2 dB per step, hold each step 20 sec, hold 14.1 G for 60 seconds
- Should consider several factors for LSF error budget
  - Astigmatism, period error, alignment (plates and modules), and thermal

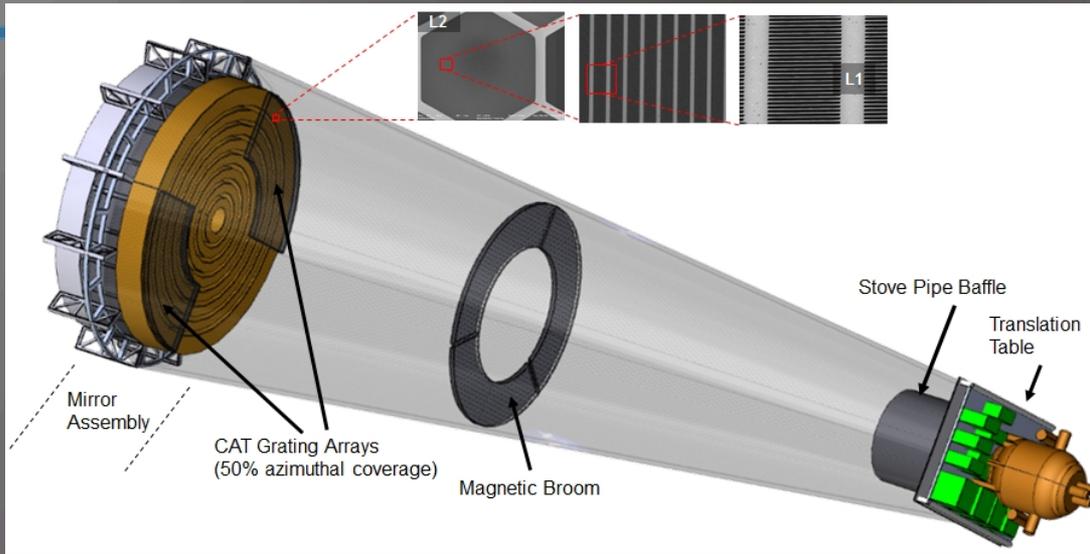


# OPG Focal Plane

- Use same technology as the HDXI
- Sensors arranged in an arc
- Zero order camera plus spectra detectors
- Example readout:
  - Assumes 10 m focal length, 0.5" telescope HPD (<24  $\mu\text{m}$  pixels), blaze wavelength 60  $\text{\AA}$  1<sup>st</sup> order, 0.5" grating induce defocus, results in  $R \sim 10,000$



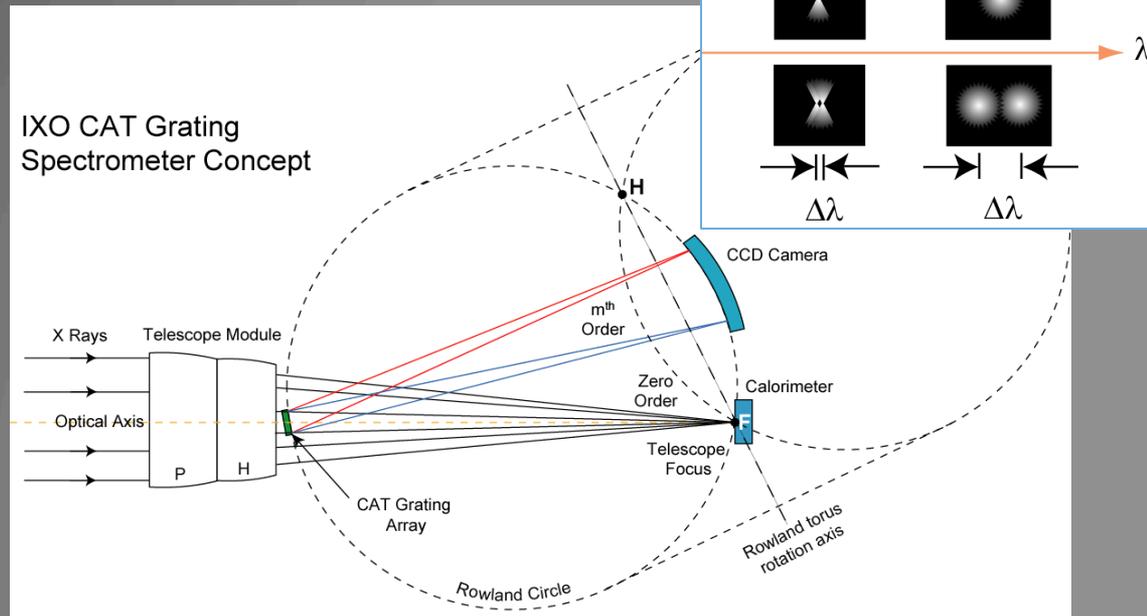
# Critical Angle Transmission Gratings (MIT)



## Advantages:

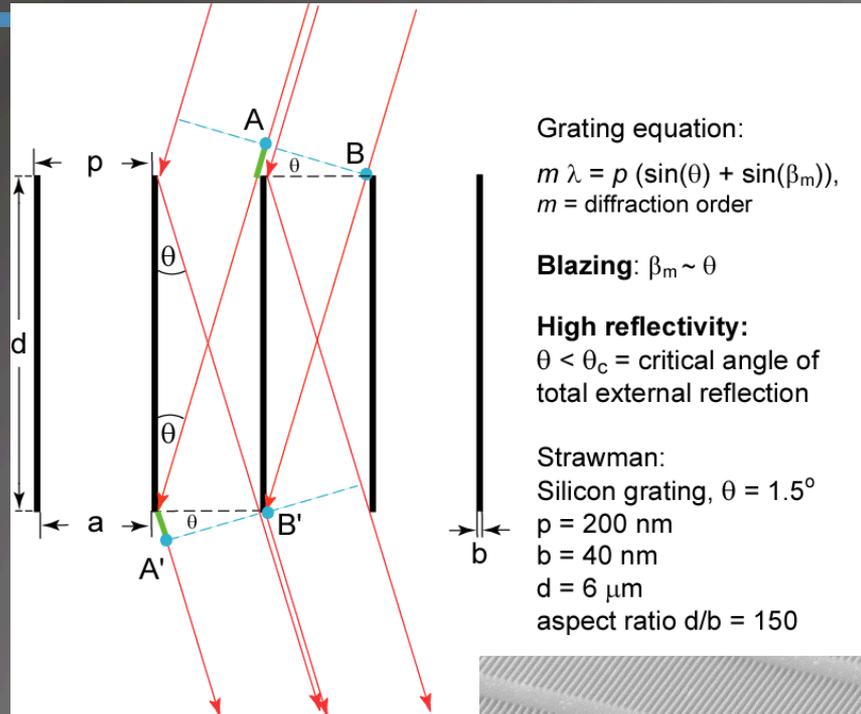
- low mass
- transparent at higher energies
- relaxed alignment & figure tolerances
- high diffraction efficiency
- demonstrated  $R > 10,000$

- Gratings, camera, and focus share same Rowland torus.
- Blazed gratings; only orders on one side are utilized (smaller detector).
- Only fraction (50%) of mirrors is covered: “sub-aperturing” boosts spectral resolution.

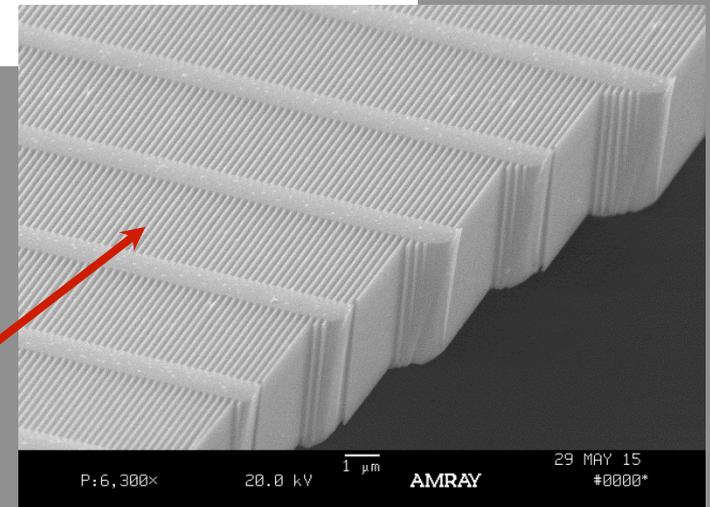


# Critical Angle Transmission Gratings (MIT)

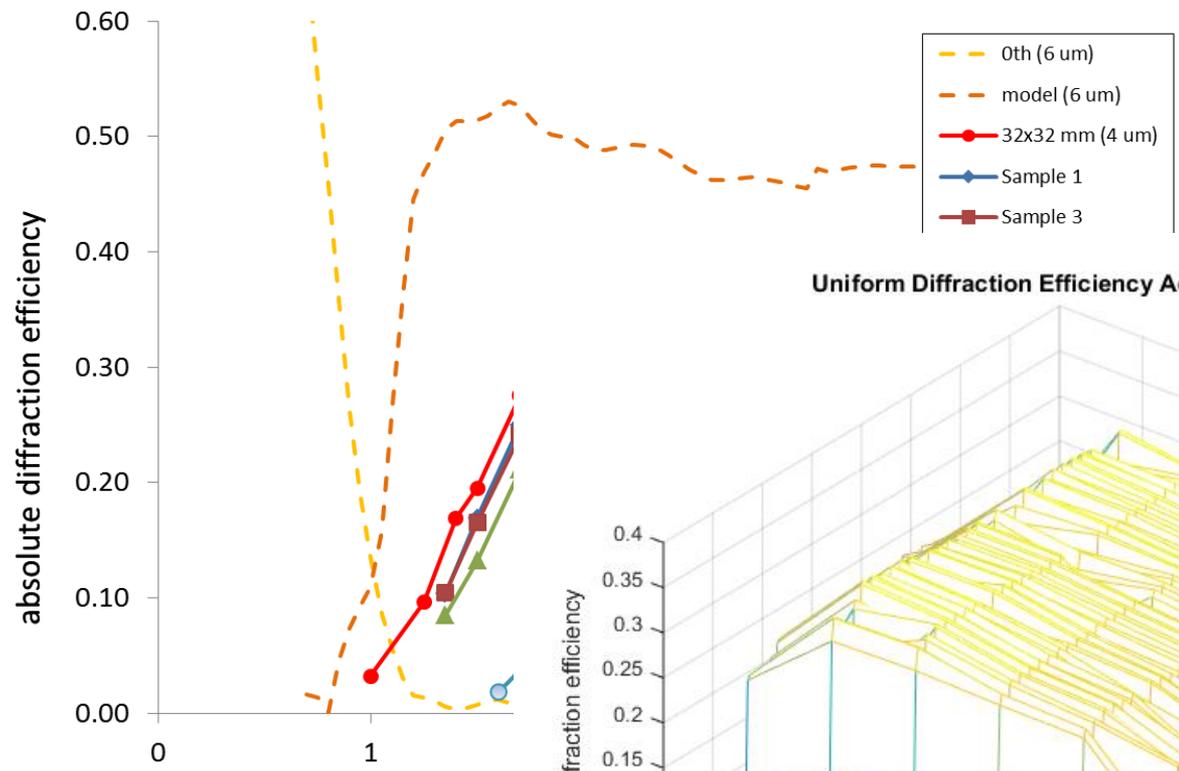
- CAT grating combines advantages of transmission gratings (relaxed alignment, low weight) with high efficiency of blazed reflection gratings.
- Blazing achieved via reflection from grating bar sidewalls at graze angles below the critical angle for total external reflection.
- High energy x rays undergo minimal absorption and contribute to effective area at focus.



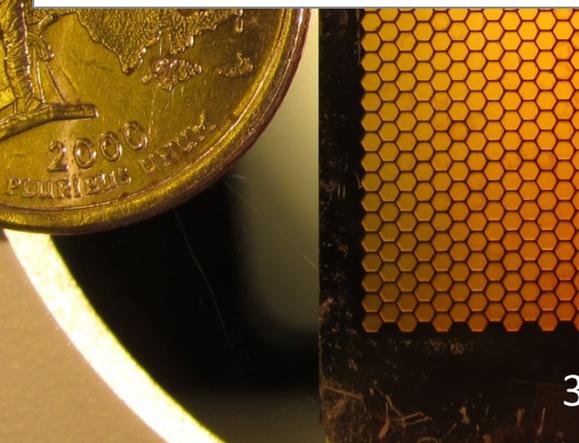
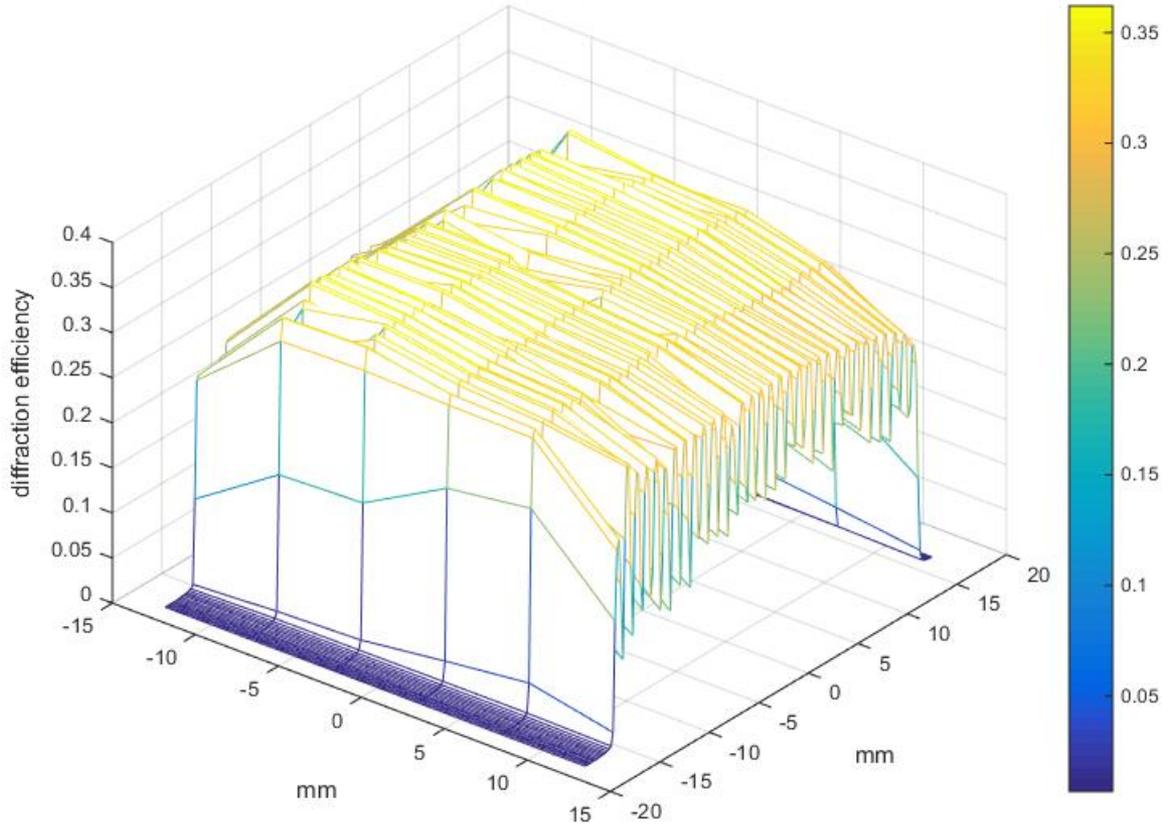
200 nm pitch  
CAT grating bars



# Recent Results



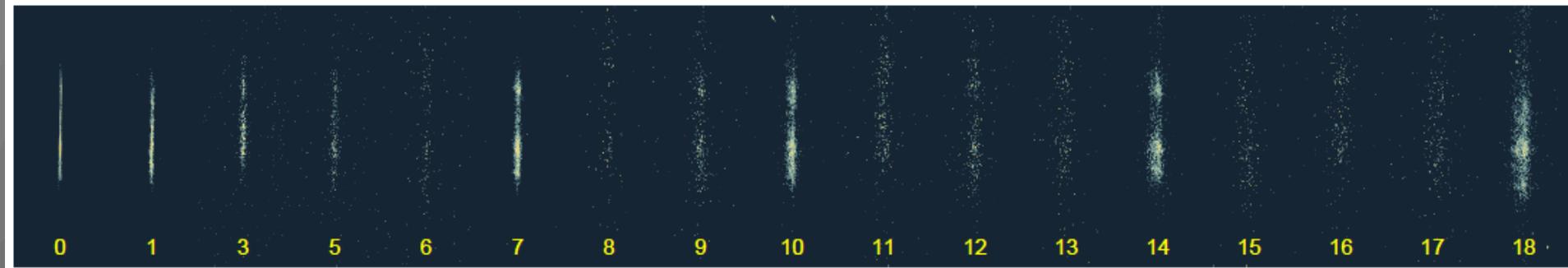
Uniform Diffraction Efficiency Across Large Grating



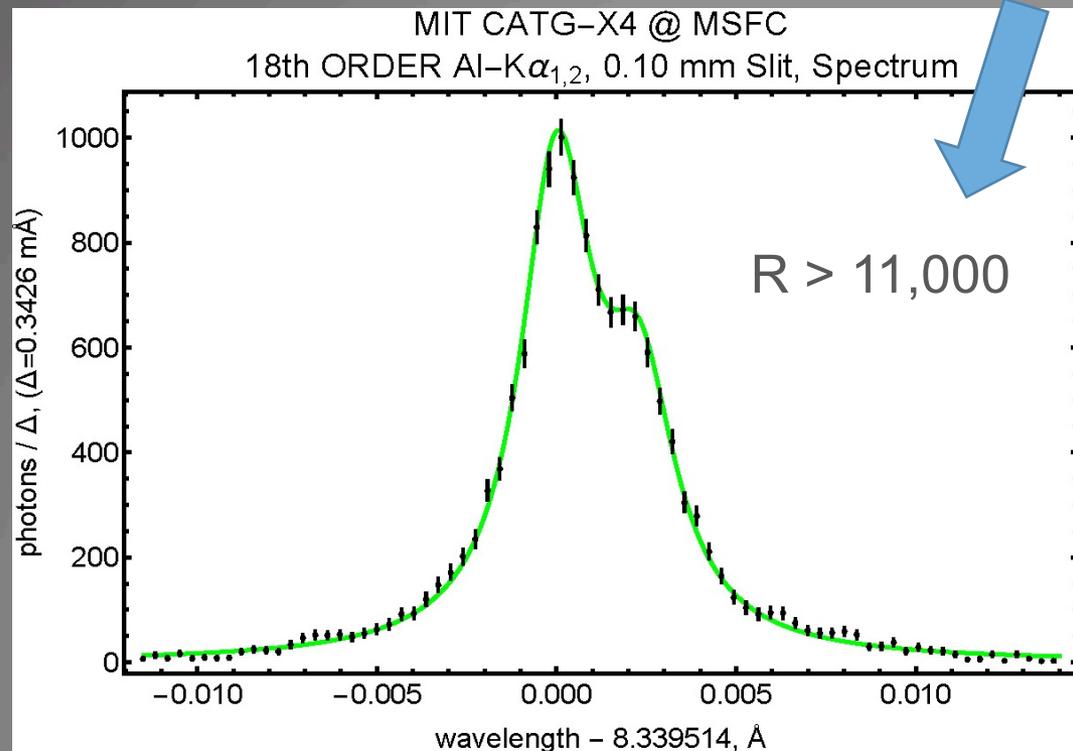
32 mm x 32 mm

# No Measurable Loss of Resolving Power

Pt-coated CAT gratings with GSFC slumped glass mirror pair:  $R > 11,000$  in 18<sup>th</sup> order at 0.834 nm



- $R \sim 24,000$  in 18<sup>th</sup> order (best fit) and  $R > 11,700$  (95% confidence) with  $\sim 1''$  mirror LSF (GSFC slumped glass P&H pair).
- $R \sim 3100$  in 9<sup>th</sup> order with first 12m-focal length SPO with  $\sim 2.5''$  optic LSF (Arcus MIDEX proposal).
- Survived shake&bake.



# Grating Trades and Needs

- Many details depend on focal length and array coverage

## Trades

- What is performance metric for each science goal?
  - Does more effective area or more resolving power make sense in each case?
- Effective area vs. resolving power
  - Telescope coverage (vs. subaperture effect)
  - Higher energy throughput vs. high blaze angle
- Detector considerations
  - High order vs. detector energy resolution
  - One readout vs. two

detection strong lines,  $W \gg \tilde{\Delta E}$ :  $M_\ell = \sqrt{\sum_{i=1}^n A_i}$

detection weak lines,  $W \ll \tilde{\Delta E}$ :  $M_\ell = \sqrt{\sum_{i=1}^n \frac{A_i}{\Delta E_i}}$

velocity strong lines,  $W \gg \tilde{\Delta E}$ :  $M_v = \sqrt{\sum_{i=1}^n \frac{E_i^2 A_i}{(\Delta E_i)^2}}$

velocity weak lines,  $W \ll \tilde{\Delta E}$ :  $M_v = \sqrt{\sum_{i=1}^n \frac{E_i^2 A_i}{(\Delta E_i)^3}}$

Jelle Kaastra for IXO

## Needs

- IDL needs: CCD readout camera, grating array mechanism, mechanical and thermal tolerances, pointing, mass, power, cost
- Technology development roadmap: SAT grants; deeper gratings, larger gratings, smaller supports, mounting and alignment schemes, coating with metals
- Other needs: Ray-tracing for resolving power and area error budgets

# Back-up slides

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