Update on the state of technology for a critical-angle x-ray transmission grating spectrometer on the X-ray Surveyor

X-ray Surveyor technology teleconference

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Why CAT Gratings?

- **Combine advantages of transmission and blazed reflection gratings:**
  - Very relaxed alignment and flatness tolerances
  - Low mass
  - Low temperature sensitivity
  - Highly transparent to high-energy x rays
  - High diffraction efficiency
  - Blazing into high orders/to large angles → high resolving power
  - Allows simple design of XGS with minimal resource requirements and orders of magnitude improved performance over existing instruments (HETGS, RGS).
Technical Background: CATXGS Design

Optical Design:
- Wolter I (or similar) telescope mirrors.
- Diffraction gratings in converging beam just aft of mirrors.
- Gratings, camera, and focus share same Rowland torus.
- Blazed gratings; only orders on one side are utilized.
- Only fraction of mirrors is covered: “sub-aperturing”.

![Diagram of CATXGS Design](image)
CAT Grating Principle

Grating equation:

\[ m \lambda = p (\sin(\theta) + \sin(\beta_m)), \]
\[ m = \text{diffraction order} \]

**Blazing:** \( \beta_m \sim \theta \)

**High reflectivity:**
\[ \theta < \theta_c = \text{critical angle of total external reflection} \]

**Strawman:**
- Silicon grating, \( \theta = 1.75^\circ \)
- \( p = 200 \text{ nm} \)
- \( b = 40 \text{ nm} \)
- \( d = 5.2 \mu\text{m} \)
- Aspect ratio \( d/b = 125 \)
Theoretical model: Rigorous Coupled-Wave Analysis (RCWA)
Parameters:
- wavelength $\lambda$
- index of refraction $n$
- period $p$
- depth $d$
- duty cycle $b$
- angle of incidence $\theta$

Absorption due to CAT grating bars already included in model, but not losses from additional structural supports (L1, L2, etc.)
Model Diffraction Efficiencies

for AEGIS design parameters

Silicon grating, $\theta = 1.75^\circ$
$p = 200$ nm
$b = 40$ nm
$d = 5.2$ $\mu$m
Aspect ratio $d/b = 125$

*AEGIS wavelength band*
Blazing at Different Wavelengths

X-ray data
Scanning wavelength:
Blaze peak width ~ \( \lambda \)
Small \( \lambda \) blaze in higher order \( m \)

\[ \lambda_c(\theta=1.14 \text{ deg}) \]
~ 0.9 nm

Blazing and Alignment Insensitivity

\[ \lambda = 6.8 \text{ nm} \]

X-ray data
“rocking” the grating:
Blaze angle \( \sim 2\theta \)
Diffraction angle \( \sim \) const.

• Boosting resolving power through sub-aperturing:
  – Sub-aperturing takes advantage of anisotropic scattering in grazing-incidence reflective optics.
  – Align dispersion direction with narrow dimension of anisotropic PSF → increase spectral resolution by factor 3-5.

Figure courtesy of D. Robinson
AEGIS as a probe-size reference mission (10” mirror PSF)

CAT Grating Structure: “Unit Cell”

(not to scale)

- Level 1 supports: (5-10 micron period)
- {111} planes: (200 nm period)
- ~ 4 - 6 um (device layer)
- ~ 500 nm (SiO2 layer)
- ~ 500 um (handle layer)
1. Start with SOI wafer

2. Pattern front and back side SiO₂

3. DRIE front side and stop on SiO₂

4. Fill front side gratings with photoresist

5. Flip over, bond to carrier wafer with crystalbond under vacuum, DRIE handle layer

6. Separate from carrier in hot water, piranha clean twice and critical-point dry

7. Remove buried SiO₂ and SiO₂ front side mask via vapor HF
CATXGS Structural Hierarchy

EXAMPLE: AEGIS

GRATING ARRAY

MIRROR ARRAY

READOUT CAMERAS

LEVEL 2 SUPPORTS

LEVEL 1 SUPPORTS

GRATING FACET (MEMBRANE & FRAME)

GRATING ARRAY STRUCTURE (GAS)
Key Performance Parameters/Technical Targets

• Grating “throughput” (effective area)
  – Flow down from science requirement for effective area.
  – Mirror design gives mirror effective area and aperture to be covered by gratings.
  – Losses reduce mirror effective area:
    o Blockage from grating support structures (GAS, facet frames (L3), L2, L1)
    o Gaps between grating facets
    o Diffraction efficiency < 100%
    o Detector size and readout/quantum efficiency
  – Realistic grating throughput goal: > 0.3

• Resolving Power
  – Flow down from science requirements
  – Requirement: \[ R = \frac{\lambda}{\Delta\lambda} = 3500 \]
  – Determined by
    o Mirror design, mirror PSF, error distribution within mirror PSF
    o Assembly and alignment errors
    o Optical design (focal length, Rowland torus parameters, sub-aperture azimuth, grating size, blaze angle)
    o Grating period variation \[ \Delta p/p \]
    o Detector pixel size
    o Thermal expansion
    o Spacecraft pointing
Technical Status

• Major milestones
  – Developed front and backside DRIE process -> freestanding gratings with narrow L1 supports
  – Integrated KOH polishing into process for smoother sidewalls
  – Confirmed theoretical diffraction efficiency predictions with synchrotron measurements over wide band of wavelengths, angles, and grating parameters (several publications in peer reviewed literature; see http://snl.mit.edu)
  – Fabricated and x-ray tested metal-coated extended-bandpass CAT gratings for resolving power measurements at MSFC Stray Light Facility (SLF)
  – Performed resolving power measurements: demonstrated $R > 10,000$

• Technology Readiness Level 4 (vetted by PCOS Technology Board)
Results

- Product: 200 nm-period silicon CAT grating membrane with integrated L1 and L2 supports, > 30x8 mm².
Recent Samples
Scanning electron micrographs of cleaved freestanding CAT grating samples
Practically defect-free large-area CAT gratings with low-duty-cycle L1 support bars
Diffraction Efficiency: ALS Beamline 6.3.2

$\lambda = 2 \text{ nm}$
• Synchrotron data: Sum of efficiencies in blazed orders, reduced by L1 absorption.
• Achieved 88% of model prediction at $\lambda = 2.5$ nm.
• Repeatable fabrication process leads to repeatable performance.

4 $\mu$m deep gratings (AEGIS design: 5.2 $\mu$m)

Extended Bandpass CAT Gratings

- Blaze angle limited by critical angle for silicon.
- Conformally coat CAT gratings with nm-thin layers of materials with higher electron density/critical angle → extended bandpass CAT gratings

$\lambda = 1.0 \text{ nm}$
$\theta = 2.0^\circ$
Grating Uniformity

- Measure diffraction efficiency of blazed order while scanning grating through the x-ray beam (red curve shifted for clarity, dips due to L2 mesh blockage)
Resolving Power

MSFC Stray Light Test facility: Al K$_α$ source ($\lambda \sim 0.83$ nm, $\lambda/\Delta \lambda \sim 3400$), ~90 m beam line
Focusing Optic: GSFC Technology Development Module (~8.5 m focal length)
Sub-apertured LSF: ~1.5” FWHM in dispersion direction
AEGIS requirement: R > 3500.
Dispersion angle 1°: R = $\lambda/\Delta \lambda \sim 2400$
Dispersion angle 3.5° (AEGIS): R = $\lambda/\Delta \lambda \sim 8400$!
Problem: $\Theta_c \sim 1.1°$ for Si CAT gratings at $\lambda = 0.83$ nm;
current 4 µm deep gratings optimized for ~2.0°
Solution: Coat Si gratings with PT using ALD -> extended band CAT gratings
MSFC SLF Optical Layout

MSFC Stray Light Facility test setup
top down view

source

mirrors

P
H

mirrors

dispersion axis

camera

~ 90 m

~ 9.25 m

CAT grating
Resolving Power

TDM and CAT gratings

0\textsuperscript{th} order image
(\sim 1.2” LSF)

18\textsuperscript{th} order image
(\sim 1.2” LSF)

CAT gratings during optical alignment
Measured Al Kα₁₂ spectrum in 18th order with 0.15 mm slit. Vertical lines are the error bars around the number of photons in a given bin. Light gray are the two Kα components with their natural Lorentzian widths, green is their sum. Blue is the convolution with the measured source/mirror 1-D LSF. Dark gray is the blue curve convolved with broadening due to a Gaussian ∆p/p distribution that would limit R to 10,000. It still falls short at the peak. The red curve also assumes a Gaussian ∆p/p distribution, but corresponding to R = 3000.

Right: Measurements of the Al Kα₁₂ spectrum with a double crystal monochromator by Schweppe et al. (J. Schweppe et al., J. Electron Spectrosc. Relat. Phenom 67, 463 (1994)).
Measured Al K$_{\alpha_{1,2}}$ spectrum with 0.10 mm slit (8 hour exposure). The green curve is a simple one-parameter fit to the sum of two Lorentzians with their quoted natural widths (0.002412 Å), a 2:1 amplitude ratio, and 0.002317 Å spacing. There is very little room for a convolution with the measured LSF (1.0") and even less room for any broadening due to contributions from the grating.

Preliminary analysis strongly suggests that the tested CAT gratings, illuminated across 30 mm width, are not a limiting factor in the design and construction of blazed transmission grating spectrometers with resolving power on the order of $R = \lambda/\Delta\lambda = 10,000$. 
Future Plans

• Performance demonstration planned
  – Demonstrate resolving power of GAS with three CAT gratings simultaneously illuminated with x rays from focusing. Perform pre and post environmental tests.
  – Demonstrate effective area with pencil-beam synchrotron measurements of individual gratings; extrapolate from diffraction efficiency and designed and measured dimensions of larger structures (L2, L3, gaps, GAS).
    o Maximize throughput for both L3 & GAS, and/or
    o Increase diffraction efficiency by making deeper gratings & narrower bars/L1/L2

• Notional schedule or timeline: TRL5 by end of 2018, based on renewal of SAT funding.
Summary

• Technology for large-area, high-resolution soft x-ray CAT grating spectrometer stands at TRL4. Rapid recent progress and performance improvements.

• Status of technology meets/exceeds TRL4 in many respects.
  – Diffraction efficiency > 85% of maximum at 0.5 keV.
  – Gratings contain full structural complexity of goal design.
  – Uniform over surface, reasonable size.
  – Demonstrated R > 10,000 possible with CAT gratings at 1.48 keV.

• Path forward
  – Clear and feasible path to TRL5.
  – Attach gratings to frames and develop alignment technology for CAT grating array (polarization of visible light, adapted from Chandra HETGS).
  – Want to improve fabrication yield and x-ray “throughput” further.
  – Proposed for SAT funding beyond 2016.